

# Effect of Cooling Rate on Microstructure of Ti-6Al-4V Alloy Produced by Direct Metal Laser Sintering

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**Abstract**—Direct metal laser sintering (DMLS) technique allows to build complex components directly from metal powder. In this work, Ti-6Al-4V samples with dimensions 10×10×10mm<sup>3</sup> were produced by the DMLS technique. Parallel and cross laser beam scanning strategies were employed. The alloy was then heat treated at 1040°C for 1h followed by cooling in water and in furnace. Samples were characterized by optical and scanning electron microscopy in addition to X-ray diffraction (XRD). The microstructural examination revealed columnar prior  $\beta$ -grains in as received condition whereas  $\alpha + \beta$  phases were observed after heat treatment, which was further confirmed by the XRD technique.

**Index Terms**—Ti-6Al-4V; Direct Metal Laser Sintering; Microstructure

## I. INTRODUCTION

DURING the last few decades titanium alloys were developed for applications requiring good corrosion resistance and high specific strength. Typical employments include medical implants and aerospace components. Traditionally, these parts are fabricated by high-cost machining of cast or wrought bulk material. Differently from this subtractive fabrication, in additive manufacturing process, components are produced directly from metal powder in layer-by-layer manner. To date, the most established additive manufacturing technique for fabrication of metallic components include (i) laser engineered net shaping-LENS,

(ii) electron beam melting-EBM and (iii) direct metal laser sintering-DMLS. In the DMLS process, laser fuses metal powder to form the desired part which is defined by a CAD model. A description of the technique can be found in ref. [1].

In comparison to the cast or forged alloys, parts produced by DMLS technique have different microstructural features which are not fully understood to date [2,3]. Thus, there is a need to evaluate influence of process parameters and post-manufacturing treatment on resulting microstructure and materials properties. In the work present, development of the microstructure in the  $\alpha + \beta$  Ti-6Al-4V alloy produced by the DMLS process and post-manufacturing treatment is investigated. Series of heat treatments were performed to investigate response of the material.

## II. EXPERIMENTAL PROCEDURE

### A. Material

DMSL Eosint EOS 270 equipment was used to produce exploratory samples (10×10×10mm<sup>3</sup>) under argon atmosphere with gas atomized Ti-6Al-4V powder (EOS Titanium Ti64 powder for EOSINT M 270 Systems). Parallel and cross laser beam scanning strategy was employed with following parameters: hatch spacing 100 $\mu$ m, layer thickness 30 $\mu$ m, laser power 170W and scanning speed 1250mm/s. Nominal chemical composition of metal powder is shown in Table 1.

Table 1 – Nominal chemical composition of metal powder.

Element	Al	V	O*	N*	C*	H*	Fe*	Ti
wt%	5.5- 6.5	3.5- 4.5	<2000	<500	<800	<120	<2500	bal

\* ppm

### B. Heat treatment and microstructural investigation

Samples were annealed for 1h above  $\beta$  phase *transus* temperature at 1040°C with subsequent cooling in furnace and in water. The heat treatments were conducted in an electric-resistant furnace in ambient atmosphere. Four conditions were studied, as shown in Table 2. Metallographic specimens were prepared by grinding with SiC paper up to 1200 mesh followed by polishing with alumina of 1 and 0.5 $\mu$ m. Samples were then etched in solution of 5mL HNO<sub>3</sub>, 3mL HF and 100mL H<sub>2</sub>O. Microstructural investigation was carried out using Olympus® BX-51M optical microscope and Philips® LX-30 scanning electron microscope.

Vickers microhardness (HV0.5) measurements were conducted using 0.5kg work load. An average value of the discrete readings from at least five measurements was taken as a representative value for the microhardness.

Table 2 – Conditions of Ti-6Al-4V samples

Sample	Scanning strategy	Heat treatment	Condition	HV0.5
I	Parallel beam	-	As received	353 ± 3
II	Cross beam	-	As received	351 ± 2
III	Cross beam	1040°C/1h	Cooling in water	394 ± 6
IV	Cross beam	1040°C/1h	Cooling in furnace	300 ± 21

### C. X-ray diffraction (XRD)

XRD measurements were performed on grinded (SiC paper 400 mesh) faces perpendicular to the deposition direction using a Philips® X'Pert Pro diffractometer in step scan mode with step size 0.013°, time per step 200s and angular interval 30-90°. CuK $\alpha$  (0.1540nm) radiation with monochromator was used at 40kV and 45mA. Spinner was employed to minimize the texture effect. Semi-quantitative analyses and phase identification were done using the X'Pert HighScore® software. XRD patterns were compared with files from ICSD database.

## III. RESULTS AND DISCUSSION

### A. Microstructural observation

Figure 1(a-b) shows three-dimensional image montage of microstructure of as received samples fabricated by (a) parallel and (b) cross scanning strategy. A checkered structure 95×95 $\mu$ m in the top view was observed, contoured with white phase. Columnar prior  $\beta$  grains ~ 2mm in length are visible in the front and the lateral view. The width of these grains is approximately 95 $\mu$ m which corresponds to the hatch spacing used in the process (100 $\mu$ m).

The microstructure of sample heat treated at 1040°C for 1h with subsequent cooling in furnace showed  $\alpha$  phase contoured by  $\beta$  phase as presented in Figure 2(a). In the insert a

backscattered electron image of the microstructure in the same sample is shown with  $\alpha$  phase (dark) and  $\beta$  phase (bright). A heat treated sample at 1040°C for 1h followed by cooling in water is shown in Figure 2(b). Due to the higher cooling rate, a refined martensitic laths structure within polygonal grains is formed. These results are in good agreement with studies conducted by Warwick *et al.*, [4], Lütjering [5] and Sallica-Leva *et al.*, [6].

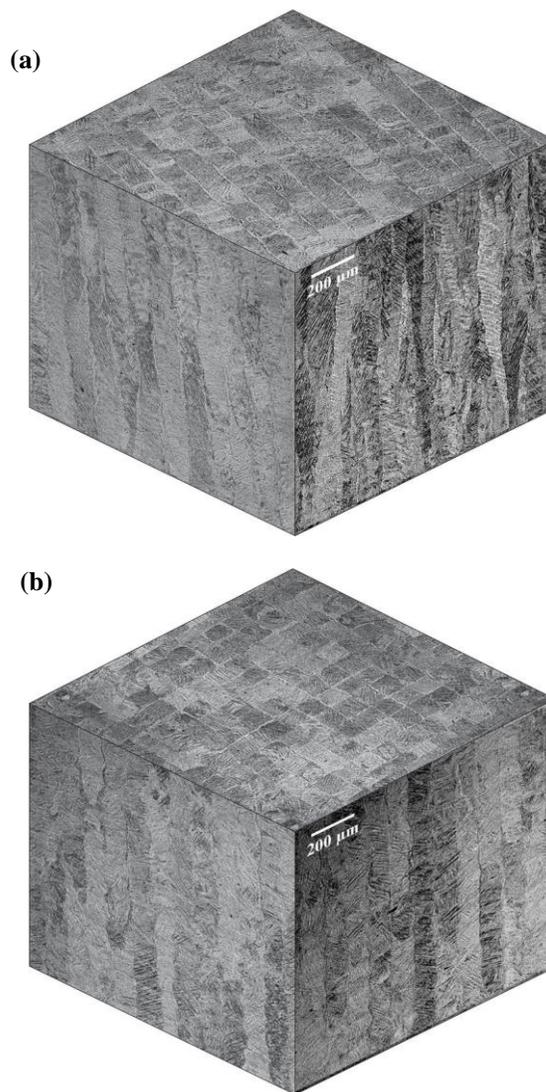


Figure 1 – 3D montage optical micrographs of as received Ti-6Al-4V samples fabricated by the DMLS technique employing (a) parallel and (b) cross scanning strategy.

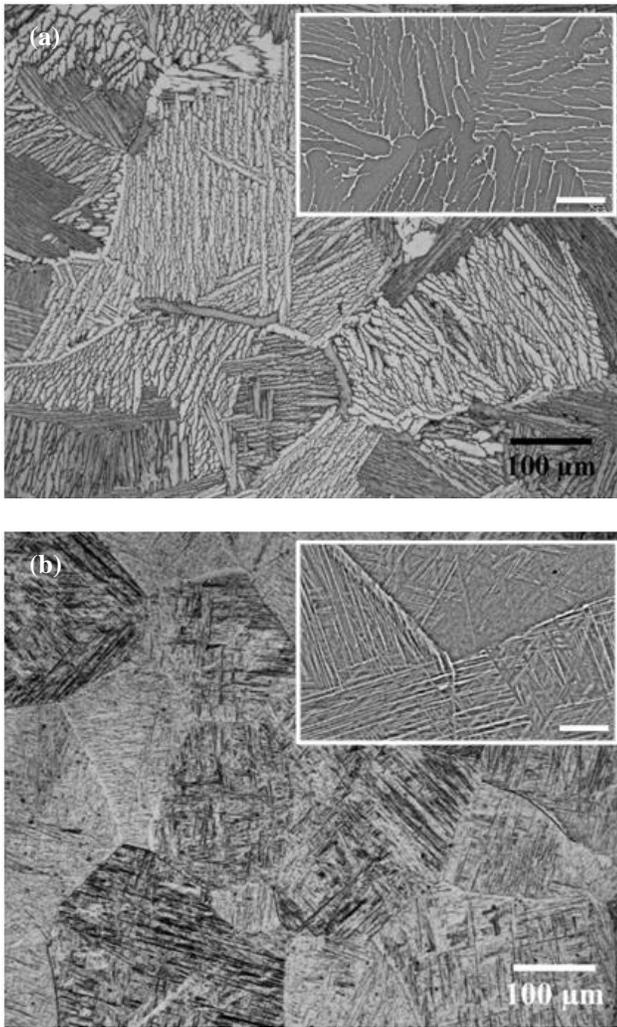


Figure 2 – Optical micrographs of heat treated Ti-6Al-4V samples at 1040°C for 1h followed by (a) furnace and (b) water cooling. In the inset a backscattered electron micrograph of the same sample is shown. The scale bar in the inset is 20μm.

### B. XRD Analysis

XRD results from Ti-6Al-4V samples are presented in the Figure 3. In the as received condition (samples I and II) an hexagonal close packed-hcp titanium  $\alpha$  phase (ICSD 43416) was identified from the XRD patterns. No difference was observed between parallel and cross beam laser scanning process. After heat treatment, the XRD patterns revealed that cooling in water (sample III) does not promote formation of  $\beta$  phase. In sample cooled in furnace (sample IV) in addition to the hcp  $\alpha$  phase presence of body crystal centered-bcc titanium  $\beta$  phase (ICSD 76165) was observed. Semi-quantitative analysis indicated a bcc  $\beta$  phase volume fraction of about 13%.

### C. Microhardness

Results of microhardness are shown in Table 2. The highest value was measured in sample heat treated at 1040°C for 1h followed by water cooling, which can be attributed to the

lower grain size and more refined martensitic structure.

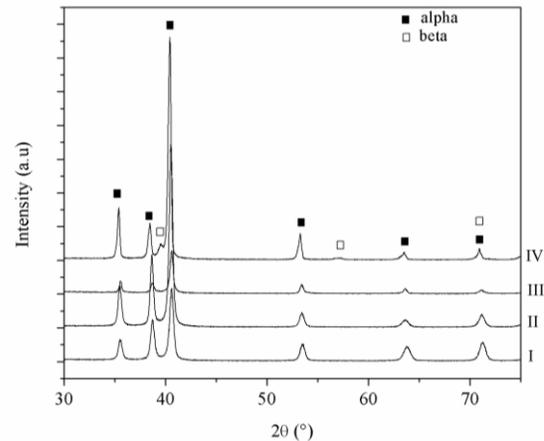


Figure 3 – XRD patterns from DMLS processed Ti-6Al-4V alloy. As received condition parallel beam (I), cross beam (II), heat treated at 1040°C for 1h and cooled in water (III) and in furnace (IV).

## IV. CONCLUSION

Ti-6Al-4V alloy was produced by DMLS technique. Based on the results of this investigation, the following conclusions can be drawn:

1. Parallel and cross laser beam strategy does not influence the final microstructure.
2. Slow cooling rate from temperature above  $\beta$  *transus* promotes growth of bcc  $\beta$  phase between  $\alpha$  laths whereas higher cooling rate results in hcp martensitic structure with high hardness.

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